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Effect of a New Absorber Design on the Performance of PV/T Collector: Numerical Comparative Study



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ARTICLE INFO	ABSTRACT
Article history: Received 27 January 2020 Received in revised form 3 April 2020 Accepted 9 April 2020 Available online 30 April 2020	The solar energy applications can be roughly divided into two main groups. A photovoltaic is an energy system that transforms solar energy into electric power and thermal energy system called solar collector that transforms solar energy into thermal energy. The photovoltaics performance affected by the high temperature of it is surface that absorbs the solar irradiance and the efficiency drop due to these higher temperatures. Therefore, the two systems associated with each other in the combined system called PV/T to enhance photovoltaic efficiency. The term PV/T (photovoltaic thermal) refers to a solar collector that uses a photovoltaic cell as an integral component of the absorption plate. The high temperature of solar photovoltaic will be decreased and transmitted to the circulated fluid inside the collector tubes. This system produces electrical and thermal at the same time. The solar collector to enhance the overall performance of the PV/T system. In the present work, a new photovoltaic thermal collector named serpen-direct is designed. Modeling for the new absorber design has been developed and validated. Numerically, PV/T performance for the serpent-direct design is analyzed and compared with the conventional serpentine design by using MATLAB Simulink. The PV and thermal efficiencies were determined under various parameters condition; mass flow rates range from 0.01 kg/s to 0.1 kg/s and solar irradiance values 700 W/m2 and 900 W/m2. Results indicate that the serpendirect flow absorber design achieved a better system overall performance than serpentine design and 14.43 %, 56.1%, correspondingly, for the serpentine absorber design.
design; Mass flow rate	Copyright © 2020 PENERBIT AKADEMIA BARU - All rights reserved

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1. Introduction

The hybrid PV/T system shown in Figure 1 is a technology that transforms solar radiation, simultaneously, into heat and electricity. This system Combine the functions of the photovoltaics and solar collectors [1]. It consists of adding a solar collector under the photovoltaic module. An absorber plate contact with the photovoltaic. In this way, the absorber plate will collect the thermal energy causing in the photovoltaic module, which results in an improvement in the electric production. This thermal energy uses to heat water or air circulating in the solar absorber [2].



Fig. 1. Photovoltaic thermal system [1]

The main advantages of the hybrid photovoltaic thermal system are:

- i. This type of system generates a greater amount of thermal and electrical energy per m2 than a separate system (thermal + photovoltaic). Therefore, it is particularly useful in situations where the roof area is reduced.
- ii. Improve the efficiency of the photovoltaic panel.
- iii. Because only one type of system is installed, rather than two, a saving in installation expenses is possible [3].

Many correlations express the temperature of the photovoltaic cell depending on climatic conditions, such as solar irradiance, ambient temperature, and wind speed. Other parameters that influence the electrical efficiency are the materials used in the system, such as the transmittance of glass roofs, the absorber plate, etc. Also, this electrical efficiency depends heavily on the solar irradiance flux over the PV panel and the type of PV module. A commercial photovoltaic module can convert from 6 to 20% of incident solar irradiance into electrical energy. Part of solar irradiance is reflected, but the remain of the absorbed solar irradiance is converted to heat, that accordingly due to the increase in the temperature of photovoltaic and reduce its efficiency. This heat extract by running water or air, moving in the back of the module, making use of thermal collectors [4].

From above, many technics have been used to develop the PV/T system to enhance photovoltaic performance. Several studies have been presented depend on a different type of PV panel [5], the type of circulating fluid (Colling medium) [6] and the absorber design of solar collector [7-8].

In the following literature will be a focus on the development of a PV/T system performance based on the development of the flow absorber design. The flow absorber design depends on the configurations of tubes under the absorber plate.

Ibrahim *et al.*, [9] have been studied the effect of several absorber designs shown in Figure 2 on the PV/T overall performance. They are using a simulation that conducted based on different parameters condition, such as, ambient temperature, mass flow rate and solar irradiance to



determine the best absorber design with the highest electrical and thermal efficiency. The Results indicate that the spiral flow absorber design has been achieved the highest performance with thermal (50.12%) and electrical (11.98%).



Fig. 2. (a) Direct absorber, (b) Oscillatory absorber, (c) Serpentine absorber, (d) Web absorber, (e) Spiral absorber [9]

An experimental study has been conducted for a new absorber design to predict the PV/T overall performance [10]. The plate and tube solar collector are integrated with a PV panel. The new absorber design has been found as simple in manufacturing compared with the other designs.

In the same direction of research, Sardouei *et al.*, [11] have been studied numerically and experimentally for different designs of PV/T solar collector. They are using CFD approach (computational fluid dynamic) to simulate the model. Experimental work was conducted to validate the results. The measurements determined under the low range of mass flow rate. The findings indicate that direct flow absorber achieved the highest temperature gradient. The results revealed that the uniform temperature distribution increases the overall performance of the PV/T. The experimental studies get more interesting from the researchers to develop the PV/T performance with new collector design. With different idea named (heat pipe pulsating) a novel PV/T design have been presented [12]. The study takes into account several parameters, such as mass flow rate, ambient temperature, solar irradiance, and inlet temperature. The results revealed to good thermal and electrical efficiencies compared with the conventional systems (PV/T and photovoltaic).

Furthermore, by using CFD approach simulation and experimental work, Zhou *et al.*, [13] have been investigating the distribution temperature in PV/T collector with serpentine absorber design. They studied the impact of parameters condition on the temperature distribution of PV/T surface,



such as absorber materials, tube configuration arrangement, and spacing tube. The results have been found that the uniform distribution temperature has more affected on the PV/T performance.

The literature Above mentioned that absorber design in PV/T system has an impact on its performance. Also, the literature showed that the mechanism of the heat transfers in the PV/T system deepened mainly on the configurations of the tubes in the flow absorber design. Based on this issue, the different PV/T absorber designs have some disadvantages such as, non-uniform distribution temperatures, low thermal efficiency and low electrical efficiency.

The developing of the new absorber design with new configuration of tubes will be improve the heat transfer mechanism between the PV module and solar collector in PV/T system. That will be overcome the problem of the non-uniform temperature of the PV surface. Meanwhile, improve the overall performance of the PV/T system.

This paper presents a report on the validation of modeling for the new absorber design in PV/T solar system named the "serpen-direct flow" as illustrated in Figure 3. The performance of the new absorber design has been analyzed and compared with the conventional serpentine absorber design under different parameters condition (solar irradiance and water mass flow rate). The thermal and electrical analysis was satisfied to evaluate the electrical and thermal efficiencies for the two-absorber design, MATLAB Simulink has been used for this purpose.





Fig. 3. Serpen-direct absorber design (a) Front view, (b) 3D diagram, (c) Front view with dimensions



2. Methodology

A Simulink by using Matlab as shown in Figure 4 conducted to calculate the PV/T performance for the new absorber design (serpen-direct) and the serpentine design based on the design parameters lists in Table 1. The mathematical model of the serpen-direct PV/T absorber design has been developed based on the new configurations of the serpen-direct flow absorber design that illustrated in Figure 3. Also, the thermal and electrical performance expressions of PV/T performance can be written as illustrated in the following subsections.



Fig. 4. Flowchart of the Matlab Simulink for the PV/T system performance evaluation

Table 1	
PV/T parameters	
Parameters	Values (unit)
Collector area	0.6372 m ²
Tube diameter	0.0127 m
Specific heat of the water	4180 J/kg °C
Absorber material	Copper
Insulation material	Polystyrene
Back insulation thickness	0.036 m
Tubes material	Copper
Absorber plate thermal conductivity	385 W/m °C
Absorber plate thickness	0.0015 m
Absorber transmittivity	0.88
Absorber absorptivity	0.95
Photovoltaic module type	Monocrystalline
Photovoltaic reference efficiency	15.5
Solar cell size	0.125 m x 0.125 m
I _{sc}	6.11 A
V _{oc}	21.6 V
I _{max}	5.55 A
V _{max}	18 V
Max power PV	100 W

2.1 Thermal Performance of the PV/T System

The thermal output performance of the PV/T system can be referred to as the ratio of useful energy gain over the solar irradiance per unit area at the same instant [14-15].

$$\eta_{thermal} = \frac{\int Q_u \, dt}{A_c \int I(t) \, dt} \tag{1}$$



where A_c is the area of collector, I(t) is the solar irradiance and Q_u is the useful heat gain, that can be expressed as follows:

$$Q_u = A_c F_r[(\alpha \tau)_n I(t) - U_L(T_{fi} - T_a)]$$
⁽²⁾

where $(\alpha \tau)_n$ is the PV/T system transmittance absorptance product , U_L is the overall losses coefficient , T_{fi} is the inlet water temperature, T_a is the ambient temperature and F_r is the removal factor of the collector, can be expression as follows [16-17].

$$F_r = \frac{m_f C_f}{A_c U_L} \times \left[1 - exp\left(-\frac{A_c U_L F'}{m_f C_f} \right) \right]$$
(3)

where m_f is the water mass flow rate, C_f is the heat capacity of water and F' is the effectiveness factor of the collector in PV/T system.

2.2 Photovoltaic Module Efficiency of the PV/T System

The PV efficiency of the PV/T collector primarily depends on the cell temperature as illustrated in the following equation [18-19].

$$\eta_{PV} = \eta_c \big[1 - 0.0045 \big(T_c - T_{ref} \big) \big] \tag{4}$$

where T_{ref} is the reference temperature and T_c is the cell temperature and η_c is the reference efficiency of the PV module.

2.3 Modelling Development of the PV/T System for the New Serpen-direct Flow Absorber Design

Figure 3 shows that the combination of two sets of parallel tubes (direct and serpentine) directly modifies the area of new absorber design (serpen-direct) absorber design of PV/T system. The solar collector area is an important element in the evaluations of thermal energy and heat removal factor as revealed in Eq. (2)-(3). These expressions were modified according to the area of serpen-direct flow absorber design. The area of solar collector for different absorber designs was calculated as follows [14]:

$$A_{c-serpentine} = L \times W \times NS \tag{5}$$

$$A_{c-direct} = L \times W \tag{6}$$

where L, W is the length and width of the collector, respectively, NS is the number of tubes segment in the serpentine configurations. Therefore, F_r , Q_u and $\eta_{thermal}$ can be expressed as follows,

Removal factor for serpen-direct flow absorber design:

 F_r will be calculated as, $F_{r-serpentine}$ determined as in [20-21] based on $A_{c-serpentine}$ calculation, and $F_{r-direct}$ can be evaluate as in Eq. (3),

$$F_{r\,serpen-direct} = \frac{F_{r-serpentine} + F_{r-direct}}{2} \tag{7}$$



Thermal energy gains for serpen-direct flow absorber design: The thermal energy for serpen-direct absorber Q_u will be written as,

$$Q_{u \, serpen-direct} = A_c \, F_{r \, serpen-direct} \left[(\alpha \tau)_n . \, I(t) - U_L \left(T_{fi} - T_a \right) \right] \tag{8}$$

Thermal performance for serpen-direct flow absorber design: The thermal efficiency of the PV/T serpen-direct flow absorber design can be evaluated as,

$$\eta_{thermal,Serpin-Direct} = \frac{\int Q_{u\,serpen-direct}\,dt}{A_c \int I(t)\,dt} \tag{9}$$

3. Results and Discussion

This section presents the analyzing of the PV/T overall performance in term of electrical and thermal efficiencies for both absorber designs (serpen-direct and serpentine). The performance has been investigated under different parameters condition, such as solar irradiance and water mass flow rate. The new model of PV/T serpen-direct has also been verified in the following section.

3.1 Model Validation

To verify the new absorber design for PV/T system (serpen-direct), we use the data collected in the previous study of Zhou *et al.*, [13] to compare the existing simulation results at the same input data with the simulation results from the previous study. The electrical values have been compared at the same operating conditions to validate the existing work Matlab Simulink (author simulation).

Figure 5 shows the difference in electrical efficiency between the simulation of the existing work and the results of previous work simulation [13] does not exceed 6.1%, the minimum percentage difference is 0.2%, and the root mean square value is 1.45%. Therefore, the results indicate the good agreement.



Fig. 5. Comparison of simulation results for electrical efficiency according to the reduced temperature between the previous study and the Author work



3.2 Effects of Mass Flow Rate and Solar Irradiance on Thermal Efficiency of the PV/T System

The mass flow rate greatly affects the thermal efficiency of the PV/T system. This section discussed the effect of various mass flow rates of water on the thermal efficiency of both (serpendirect and serpentine) flow absorber designs. Figure 6 compares the difference in thermal efficiency between the two designs with the increase in water flow rate at 700 W/m2. The thermal efficiency of both absorber designs increases with increasing mass flow rate, taking into account the relative relationship between water flow rate and thermal efficiency as specified in Eq. (1)-(2).

In Figure 6 and Figure 7 by increasing the solar irradiance from 700 W/m2 to 900 W/m2 with same mass flow rate, the thermal efficiency increases for both absorber design (serpentine and serpen-direct). It can be noted that at 0.012 kg/s in Figure 6 the thermal efficiencies were 50% and 49.5% for serpen-direct and serpentine absorber, respectively. After that, with 0.058 kg/s mass flow rate the thermal efficiencies increase to achieved 52.2% and 53.5% for the serpen-direct and serpentine absorber, correspondingly. Also, it can be noted that there is no significant change in the description of the effect of the mass flow rate of thermal efficiency in Figure 7, including solar irradiance of 900 W/m2. Furthermore, it can be seen that the thermal efficiency is higher in a serpentine flow design than in a serpen-direct flow design with a mass flow rate greater than 0.012 kg/s.



Fig. 6. Effects of mass flow rate variation on thermal efficiency at solar irradiance 700 W/m2





Fig. 7. Effects of mass flow rate variation on thermal efficiency at solar irradiance 900 W/m2

3.3 Effects of Mass Flow Rate and Solar Irradiance on the PV Efficiency of the PV/T System

The effect of mass flow rate on photovoltaic efficiency related to solar cell temperature. The temperature of the PV surface decreases as the mass flow rate increases. That led to a direct impact on PV efficiency as expressed in Eq. (4).

Figure 8 shows the photovoltaic efficiencies at different mass flow rates and 700 W/m2 solar irradiance. The results show that the PV efficiency of two design increases with increasing mass flow rate. The PV module efficiency achieved 14.37% and 14.31% for PV/T serpen-direct and serpentine flow absorber, respectively, with a flow rate of 0.012 kg/s. Besides, the PV efficiencies at mass flow rates increasing from 0.012 kg/s to 0.058 kg/s were 14.47% and 14.42%, respectively, for the PV/T serpen-direct and serpentine flow absorber.

In the results in Figure 9 show that the photovoltaic efficiency values are 13.37% and 13.84% for PV/T serpentine and serpen-direct absorber, respectively, with 0.012 kg/s and 900 W/m2, respectively. Also, as the water flow rate increases to 0.058 kg/s, the PV/T serpentine and serpen-direct absorber photovoltaic efficiency increase by 13.78% and 14.18%, respectively. These results indicate that PV efficiency in serpen-direct design higher than serpentine design.

From the above, it is obvious two facts, firstly that photovoltaic efficiency increased with mass flow rate increase because of the increase in the heat transfer between the solar panel and the circulating water inside the tubes of solar collector. Secondly, that the PV efficiency drops with higher solar irradiance due to higher cell temperature obtained with higher solar irradiance.





Fig. 8. Effects of mass flow rate variation on PV efficiency at solar irradiance 700 W/m2



Fig. 9. Effects of mass flow rate variation on PV efficiency at solar irradiance 900 W/m2

4. Conclusions

The performance of the PV/T system was determined based on various absorber designs, and a comparative study of system performance was performed. The results showed that the performance of the PV/T collector could be improved by increasing the mass flow rate of water. The maximum efficiency of photovoltaic is 14.52% and 14.43%, respectively, with a flow rate of 0.098 kg/s and solar radiation of 700 W/m2, respectively. Also, at optimized parameters condition, mass flow rate 0.012 kg/s and 900 W/m2 solar radiation, the thermal performance of both PV/T designs serpen-direct and serpentine were found 51% and 50.7%, correspondingly. These results show that serpen-direct flow absorber design works better than serpentine absorber in PV/T systems.



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